

Network Systems and Kuramoto Oscillators

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2018 President, IEEE Control Systems Society
A kind invitation to participate in CSS activities



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Acknowledgments



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National Renewable Energy Laboratory, UCSB and University of Minnesota



Outline

1 Intro to Network Systems and Power Flow

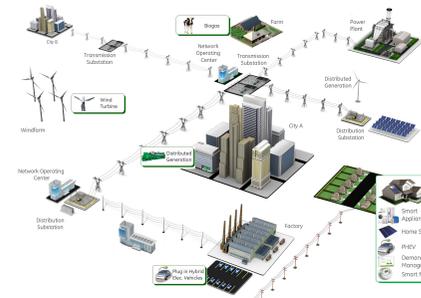
Known tests and a conjecture

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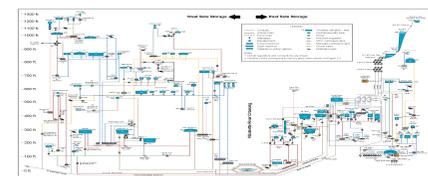
Example network systems



Smart grid



Amazon robotic warehouse

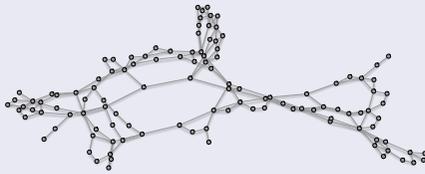


Portland water network



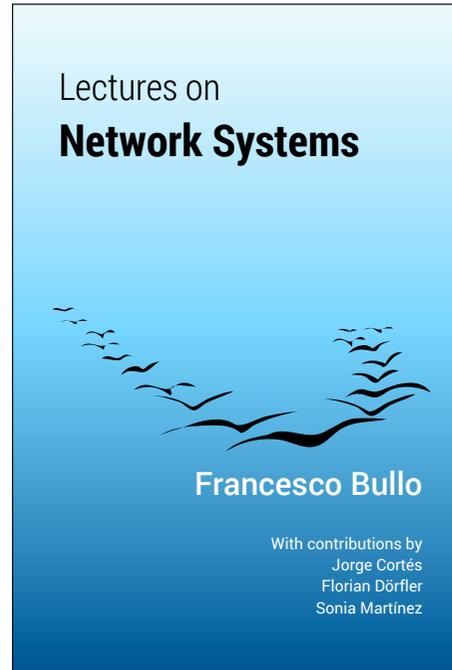
Industrial chemical plant

$$x(k + 1) = Ax(k) + b \quad \text{or} \quad \dot{x}(t) = Ax(t) + b$$



- 1 systems of interest
- 2 asymptotic behavior
- 3 tools

network structure \iff function = asymptotic behavior



Lectures on Network Systems, 1 edition
ISBN 978-1-986425-64-3

For students: free PDF for download
For instructors: slides and answer keys
<http://motion.me.ucsb.edu/book-lns>
<https://www.amazon.com/dp/1986425649>
300 pages (plus 200 pages solution manual)
3K downloads since Jun 2016
150 exercises with solutions

Linear Systems:

- 1 social, sensor, robotic & compartmental examples,
- 2 matrix and graph theory, with an emphasis on Perron–Frobenius theory and algebraic graph theory,
- 3 averaging algorithms in discrete and continuous time, described by static and time-varying matrices, and
- 4 positive & compartmental systems, dynamical flow systems, Metzler matrices.

Nonlinear Systems:

- 1 nonlinear consensus models,
- 2 population dynamic models in multi-species systems,
- 3 coupled oscillators, with an emphasis on the Kuramoto model and models of power networks

Synchronization in Networks of Coupled Oscillators

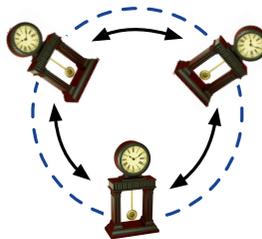
Pendulum clocks & “an odd kind of sympathy”
[C. Huygens, Horologium Oscillatorium, 1673]

Today’s canonical coupled oscillator model
[A. Winfree '67, Y. Kuramoto '75]

Coupled oscillator model:

$$\dot{\theta}_i = \omega_i - \sum_{j=1}^n a_{ij} \sin(\theta_i - \theta_j)$$

- n oscillators with phase $\theta_i \in \mathbb{S}^1$
- **non-identical** natural frequencies $\omega_i \in \mathbb{R}^1$
- **coupling** with strength $a_{ij} = a_{ji}$



Synchronization in Networks of Coupled Oscillators applications

Coupled oscillator model:

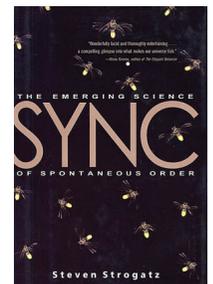
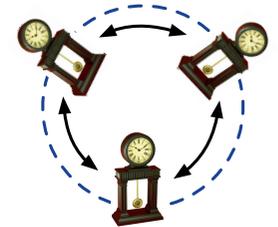
$$\dot{\theta}_i = \omega_i - \sum_{j=1}^n a_{ij} \sin(\theta_i - \theta_j)$$

A few related applications:

- Sync in Josephson junctions
[S. Watanabe et. al '97, K. Wiesenfeld et al. '98]
- Sync in a population of fireflies
[G.B. Ermentrout '90, Y. Zhou et al. '06]
- Canonical model of coupled limit-cycle oscillators
[F.C. Hoppensteadt et al. '97, E. Brown et al. '04]
- Countless sync phenomena in sciences/bio/tech.
[A. Winfree '67, S.H. Strogatz '00, J. Acebrón '01]

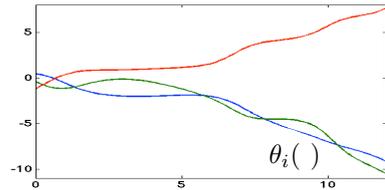
citations on scholar.google:

Kuramoto oscillators 1.4K, synchronization

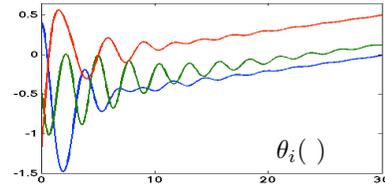


Function = synchronization

$$\dot{\theta}_i = \omega_i - \sum_{j=1}^n a_{ij} \sin(\theta_i - \theta_j)$$



coupling small & $|\omega_i - \omega_j|$ large
 \Rightarrow incoherence = no sync



coupling large & $|\omega_i - \omega_j|$ small
 \Rightarrow coherence = frequency sync

Central question:

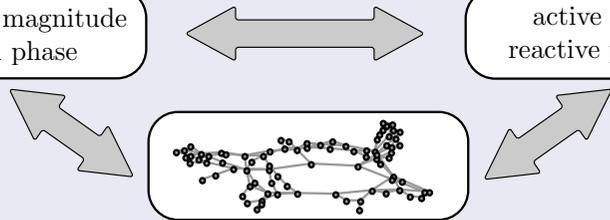
[S. Strogatz '01, A. Arenas et al. '08, S. Boccaletti et al. '06]

- loss of sync due to bifurcation
- trade-off “coupling” vs. “heterogeneity”
- how to quantify this trade-off

Power flow equations

voltage magnitude and phase

active and reactive power



- 1 secure operating conditions
- 2 feedback control
- 3 economic optimization

network structure \iff function = power transmission

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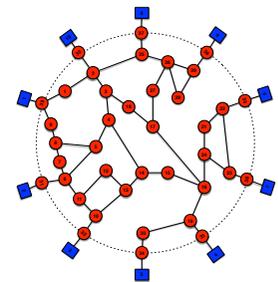
Power networks as quasi-synchronous AC circuits

1 generators ■ and loads ●

2 physics: Kirchoff and Ohm laws

3 today's simplifying assumptions:

- 1 quasi-sync: voltage and phase V_i, θ_i
active and reactive power p_i, q_i
- 2 lossless lines
- 3 approximated decoupled equations



Decoupled power flow equations

active: $p_i = \sum_j a_{ij} \sin(\theta_i - \theta_j)$

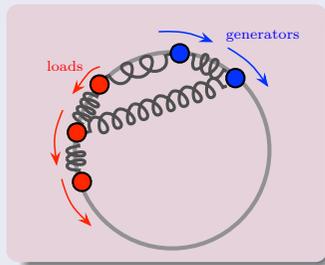
reactive: $q_i = -\sum_j b_{ij} V_i V_j$

$$p_i = \sum_j a_{ij} \sin(\theta_i - \theta_j)$$

As function of network structure/parameters

- 1 do equations admit solutions / operating points?
- 2 how much active power can network transmit / flow?
- 3 how to quantify stability margins?

Active power dynamics and mechanical/spring analogy



Coupled swing equations

$$m_i \ddot{\theta}_i + d_i \dot{\theta}_i = p_i - \sum_j a_{ij} \sin(\theta_i - \theta_j)$$

Kuramoto coupled oscillators

$$\dot{\theta}_i = p_i - \sum_j a_{ij} \sin(\theta_i - \theta_j)$$

Sync is crucial for the functionality and operation of the AC power grid. Generators have to swing in sync despite fluctuations/faults/contingencies.

Given: network parameters & topology and load & generation profile

Q: “ \exists an optimal, stable, and robust synchronous operating point ?”

- 1 Security analysis [Araposthatis et al. '81, Wu et al. '80 & '82, Ilić '92, ...]
- 2 Load flow feasibility [Chiang et al. '90, Dobson '92, Lesieutre et al. '99, ...]
- 3 Optimal generation dispatch [Lavaei et al. '12, Bose et al. '12, ...]
- 4 Transient stability [Sastry et al. '80, Bergen et al. '81, Hill et al. '86, ...]
- 5 Inverters in microgrids [Chandorkar et al. '93, Guerrero et al. '09, Zhong '11, ...]

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Primer on algebraic graph theory

Weighted undirected graph with n nodes and m edges:

Incidence matrix: $n \times m$ matrix B s.t. $(B^T p_{\text{active}})_{(ij)} = p_i - p_j$

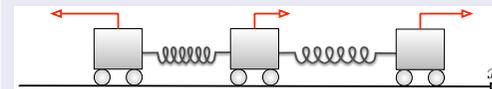
Weight matrix: $m \times m$ diagonal matrix \mathcal{A}

Laplacian stiffness: $L = B\mathcal{A}B^T$

Kuramoto eq points: $p_{\text{active}} = B\mathcal{A} \sin(B^T \theta)$

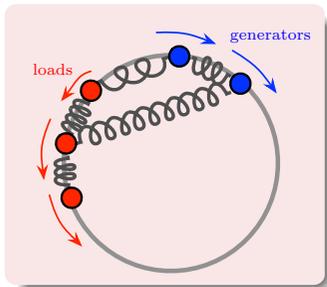
Algebraic connectivity: $\lambda_2(L) =$ second smallest eig of L

Linear spring networks and L^\dagger



$$f_i = \sum a_{ij} (x_j - x_i) = -(Lx)_i$$

$$x = L^\dagger f \quad \text{for balanced } f \perp \mathbb{1}_n$$



Given balanced p_{active} , do angles exist?

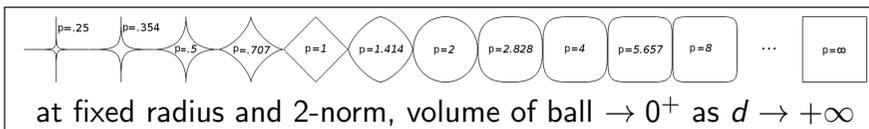
$$p_{\text{active}} = BA \sin(B^T \theta)$$

synchronization arises if
power transmission < connectivity strength

Equilibrium angles (neighbors within $\pi/2$ arc) exist if

$$\|B^T p_{\text{active}}\|_2 < \lambda_2(L) \quad \text{for unweighted graphs} \quad (\text{Old 2-norm T})$$

$$\|B^T L^\dagger p_{\text{active}}\|_\infty < 1 \quad \text{for trees, complete} \quad (\text{Old } \infty\text{-norm T})$$



$\|B^T L^\dagger p_{\text{active}}\|_\infty < 1$ appears to imply:

- 1 \exists solution θ^*
- 2 $|\theta_i^* - \theta_j^*| \leq \arcsin(\|B^T L^\dagger p_{\text{active}}\|_\infty)$ for all $\{i, j\} \in \mathcal{E}$

Randomized test case (1000 instances)	Numerical worst-case angle differences: $\max_{\{i,j\} \in \mathcal{E}} \theta_i^* - \theta_j^* $	Analytic prediction of angle differences: $\arcsin(\ B^T L^\dagger p_{\text{active}}\ _\infty)$	Accuracy of condition: $\max_{\{i,j\} \in \mathcal{E}} \theta_i^* - \theta_j^* - \arcsin(\ B^T L^\dagger p_{\text{active}}\ _\infty)$
9 bus system	0.12889 rad	0.12885 rad	$4.1218 \cdot 10^{-5}$ rad
IEEE 14 bus system	0.16622 rad	0.16594 rad	$2.7995 \cdot 10^{-4}$ rad
IEEE RTS 24	0.22309 rad	0.22139 rad	$1.7089 \cdot 10^{-3}$ rad
IEEE 30 bus system	0.1643 rad	0.16404 rad	$2.6140 \cdot 10^{-4}$ rad
New England 39	0.16821 rad	0.16815 rad	$6.6355 \cdot 10^{-5}$ rad
IEEE 57 bus system	0.20295 rad	0.18232 rad	$2.0630 \cdot 10^{-2}$ rad
IEEE RTS 96	0.24593 rad	0.245332 rad	$2.6076 \cdot 10^{-3}$ rad
IEEE 118 bus system	0.23524 rad	0.23464 rad	$5.9959 \cdot 10^{-4}$ rad
IEEE 300 bus system	0.43204 rad	0.43151 rad	$5.2618 \cdot 10^{-4}$ rad
Polish 2383 bus system	0.25144 rad	0.24723 rad	$4.2183 \cdot 10^{-3}$ rad

IEEE test cases: 50 % randomized loads and 33 % randomized generation

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$$\|B^T p_{\text{active}}\|_2 < \lambda_2(L) \quad \text{for unweighted graphs} \quad (\text{Old 2-norm T})$$

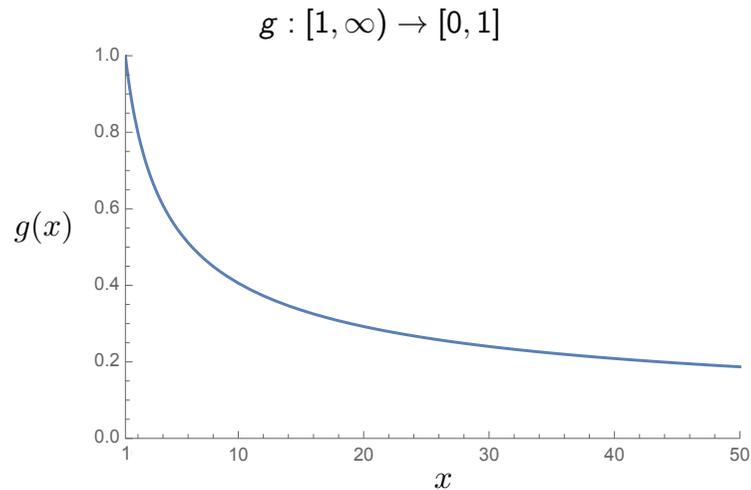
$$\|B^T L^\dagger p_{\text{active}}\|_\infty < 1 \quad \text{for trees, complete} \quad (\text{Old } \infty\text{-norm T})$$

Equilibrium angles (neighbors within $\pi/2$ arc) exist if

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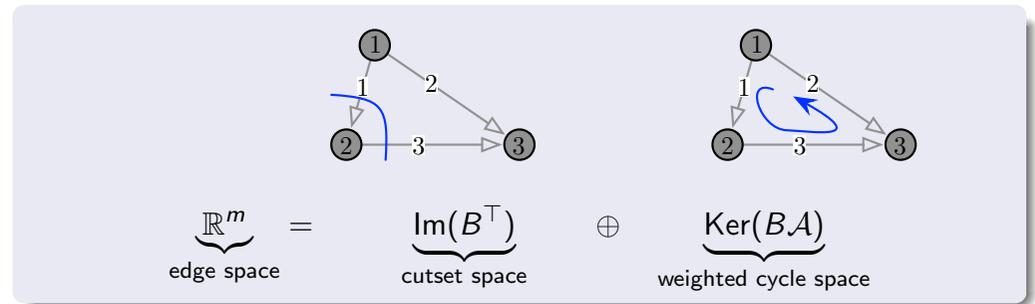
$$\|B^T L^\dagger p_{\text{active}}\|_\infty < g(\|P\|_\infty) \quad \text{for all graphs} \quad (\text{New } \infty\text{-norm T})$$

where g is monotonically decreasing



$$g(x) = \frac{y(x) + \sin(y(x))}{2} - x \frac{y(x) - \sin(y(x))}{2} \Big|_{y(x)=\arccos\left(\frac{x-1}{x+1}\right)}$$

and where \mathcal{P} is a projection



$$\mathcal{P} = B^\top L^\dagger B A = \text{oblique projection onto } \text{Im}(B^\top) \text{ parallel to } \text{Ker}(BA)$$

(recall: orthogonal projector onto $\text{Im}(C)$ is $C(C^\top C)^{-1}C^\top$ for full rank C)

- 1 if G unweighted, then \mathcal{P} is orthogonal and $\|\mathcal{P}\|_2 = 1$
- 2 if G acyclic, then $\mathcal{P} = I_m$ and $\|\mathcal{P}\|_p = 1$
- 3 if G uniform complete or ring, then $\|\mathcal{P}\|_\infty = 2(n-1)/n \leq 2$

Unifying Theorem

Equilibrium angles (neighbors within γ arc) exist if, in some p -norm,

$$\|B^\top L^\dagger p_{\text{active}}\|_p \leq \gamma \alpha_p(\gamma) \quad \text{for all graphs} \quad (\text{New } p\text{-norm T})$$

$\alpha_p(\gamma) := \min$ amplification factor of $\mathcal{P}[\text{sinc}(x)]$

For unweighted $p = 2$, new test sharper than old

$$\|B^\top L^\dagger p_{\text{active}}\|_2 \leq \sin(\gamma) \quad (\text{New 2-norm T})$$

For $p = \infty$, new test is for all graphs

$$\|B^\top L^\dagger p_{\text{active}}\|_\infty \leq g(\|\mathcal{P}\|_\infty) \quad (\text{New } \infty\text{-norm T})$$

Comparison of sufficient and approximate sync tests

K_c = critical coupling of Kuramoto model, computed via MATLAB *fsolve*
 K_T = smallest value of scaling factor for which test T fails

Test Case	Critical ratio K_T/K_c				
	old 2-norm conjectured	new 2-norm conjectured	new ∞ -norm	old ∞ -norm approximate	α_∞ test <i>fmincon</i>
IEEE 9	16.54 %	59.06 %	73.74 %	92.13 %	85.06 % [†]
IEEE 14	8.33 %	42.27 %	59.42 %	83.09 %	81.32 % [†]
IEEE RTS 24	3.86 %	35.62 %	53.44 %	89.48 %	89.48 % [†]
IEEE 30	2.70 %	40.98 %	55.70 %	85.54 %	85.54 % [†]
IEEE 39	2.97 %	37.32 %	67.57 %	100 %	100 % [†]
IEEE 57	0.36 %	31.93 %	40.69 %	84.67 %	—*
IEEE 118	0.29 %	24.61 %	43.70 %	85.95 %	—*
IEEE 300	0.20 %	24.13 %	40.33 %	99.80 %	—*
Polish 2383	0.11 %	13.93 %	29.08 %	82.85 %	—*

[†] *fmincon* has been run for 100 randomized initial phase angles.

* *fmincon* does not converge.

For what $B, \mathcal{A}, p_{\text{active}}$ does there exist θ solution to:

$$p_{\text{active}} = B\mathcal{A}\sin(B^\top\theta)$$

For what projection \mathcal{P} and flow z in cutset space, does there exist x in cutset spacesolution to:

$$\begin{aligned} z = \mathcal{P}\sin(x) &\iff z = \mathcal{P}[\text{sinc}(x)]x \\ &\iff x = (\mathcal{P}[\text{sinc}(x)])^{-1}z =: h(x) \end{aligned}$$

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- 1 look for x solving

$$x = h(x) = (\mathcal{P}[\text{sinc}(x)])^{-1}z$$

- 2 take p norm, define **min amplification factor** of $\mathcal{P}[\text{sinc}(x)]$:

$$\alpha_p(\gamma) := \min_{\|x\|_p \leq \gamma} \min_{\|y\|_p=1} \|\mathcal{P}[\text{sinc}(x)]y\|_p$$

If $\|z\|_p \leq \gamma\alpha_p(\gamma)$ and $x \in \mathcal{B}_p(\gamma) = \{x \mid \|x\|_p \leq \gamma\}$, then

$$\begin{aligned} \|h(x)\|_p &\leq \max_x \max_y \|(\mathcal{P}[\text{sinc}(x)])^{-1}y\|_p \cdot \|z\|_p \\ &\leq \frac{\|z\|_p}{\alpha_p(\gamma)} \leq \gamma \end{aligned}$$

hence $h(x) \in \mathcal{B}_p(\gamma)$ and h satisfies Brouwer on $\mathcal{B}_p(\gamma)$

Computational method via power series

Given z , compute x solution to

$$z = \mathcal{P}\sin(x)$$

Assume $x = \sum_{i=0}^{\infty} A_{2i+1}(z)$, where $A_{2i+1}(z)$ is homogeneous degree $2i+1$

$$z = \mathcal{P} \sum_{k=0}^{\infty} \frac{(-1)^k}{(2k+1)!} x^{\circ 2k+1} = \mathcal{P} \sum_{k=0}^{\infty} \frac{(-1)^k}{(2k+1)!} \left(\sum_{i=0}^{\infty} A_{2i+1}(z) \right)^{\circ 2k+1}$$

Equate left-hand and right-hand side at order $1, 3, \dots, 2j+1$:

$$A_1(z) = z$$

$$A_{2j+1}(z) = \mathcal{P} \left(\sum_{k=1}^j \frac{(-1)^{k+1}}{(2k+1)!} \sum_{\substack{\text{odd } \alpha_1, \dots, \alpha_{2k+1} \text{ s.t.} \\ \alpha_1 + \dots + \alpha_{2k+1} = 2j+1}} A_{\alpha_1}(z) \circ \dots \circ A_{\alpha_{2k+1}}(z) \right)$$

Unique solution to $z = \mathcal{P} \sin(x)$ is

$$x = \sum_{i=0}^{\infty} A_{2i+1}(z)$$

$$A_1(z) = z = B^\top L^\dagger p_{\text{active}}$$

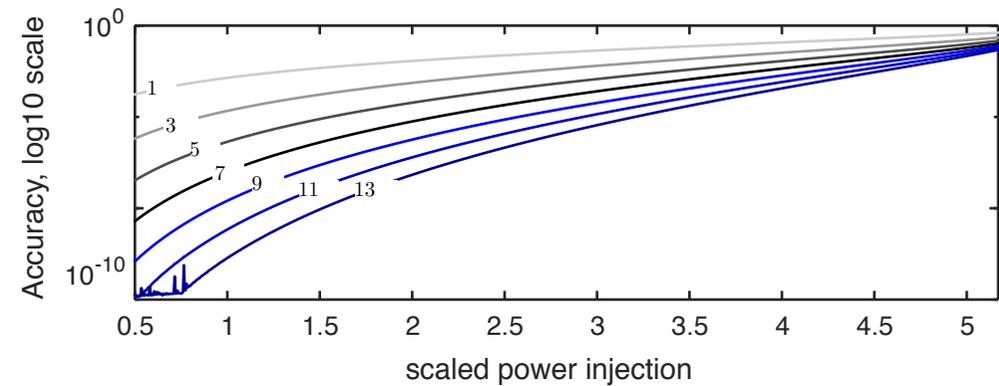
$$A_3(z) = \mathcal{P}\left(\frac{1}{3!}z^{\circ 3}\right)$$

$$A_5(z) = \mathcal{P}\left(\frac{3}{3!}A_3(z) \circ z^{\circ 2} - \frac{1}{5!}z^{\circ 5}\right)$$

$$A_7(z) = \mathcal{P}\left(\frac{3}{3!}A_5(z) \circ z^{\circ 2} + \frac{3}{3!}A_3(z)^{\circ 2} \circ z - \frac{5}{5!}A_3(z) \circ z^{\circ 4} + \frac{1}{7!}z^{\circ 7}\right)$$

arbitrary higher-order terms can be computed symbolically

Test case: IEEE 118



For sufficiently small $\|z\|_p$, series converges uniformly absolutely

Kuramoto Oscillators and Power Flow

New physical insight

- 1 sharp sufficient conditions for equilibria
 - upper bounds on transmission capacity
 - stability margins as notions of distance from bifurcations
- 2 new computational methods via power series

Applications

- 1 secure operating conditions: **(Dörfler et al, PNAS '13)**
- 2 feedback control: **(Simpson-Porco et al, TIE '15)**
- 3 economic optimization: **(Todescato et al, TCNS '17)**

Future research

- 1 close the gap between sufficient and necessary conditions
- 2 more realistic coupled power flow equations
- 3 applications to other flow networks (water, gas ...)